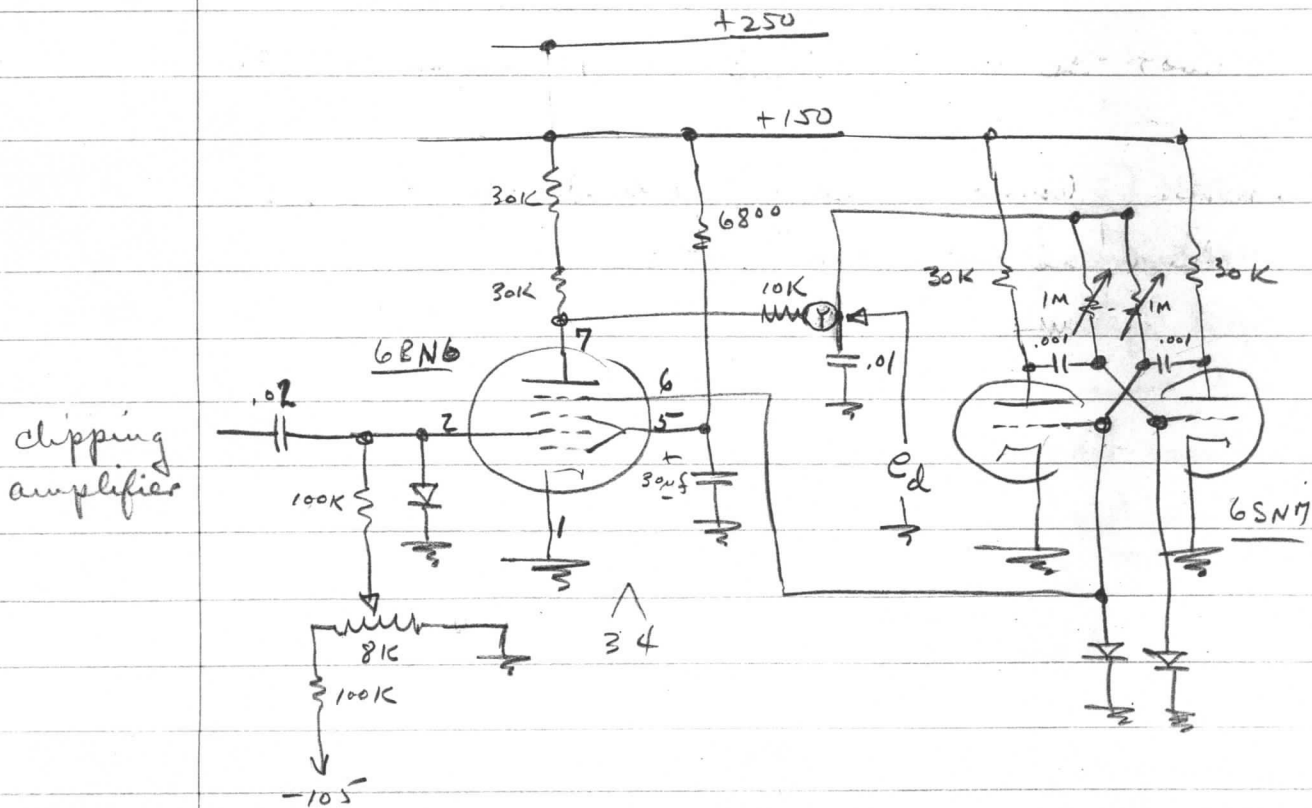
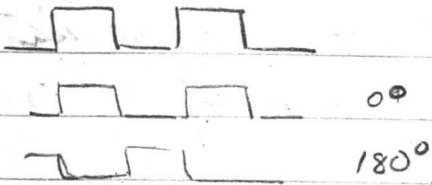


5/9/65 In the scheme of p 59 for the phase locked loop - it is apparent that the use of cathode bias lowers the drive from the MV and reference channels instead of establishing a level for reference fading. I think this accounts for the extremely low output. If the plate of the 6BN6 were returned to +250 a swing of $100V/180^{\circ}$ should be realized.



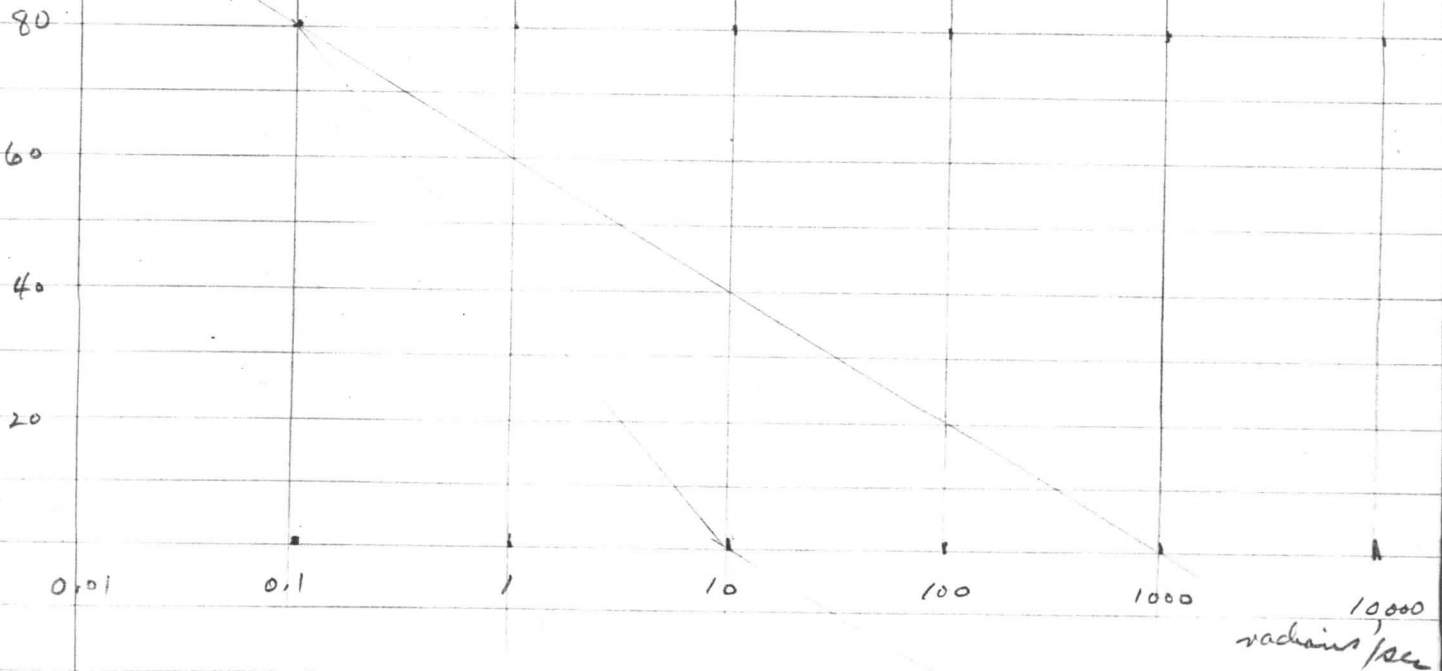
$$\frac{e_2}{\phi} = \frac{90v - 53v}{180^\circ} = \frac{36v}{\pi} = 11.5 \text{ v/radian}$$

From p89 $V_{CO} \frac{f}{e_2} = \frac{89 \text{ rad/sec}}{\text{volt}}$



$$\text{Loop gain} = \frac{89 \text{ rad/sec}}{\text{volt}} \times 11.5 \frac{\text{volt}}{\text{radian}} = 1020 / \text{sec}$$

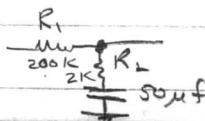
Assuming 6BN6 has very large plate resistance, source impedance is $60K + 10K = 70K$



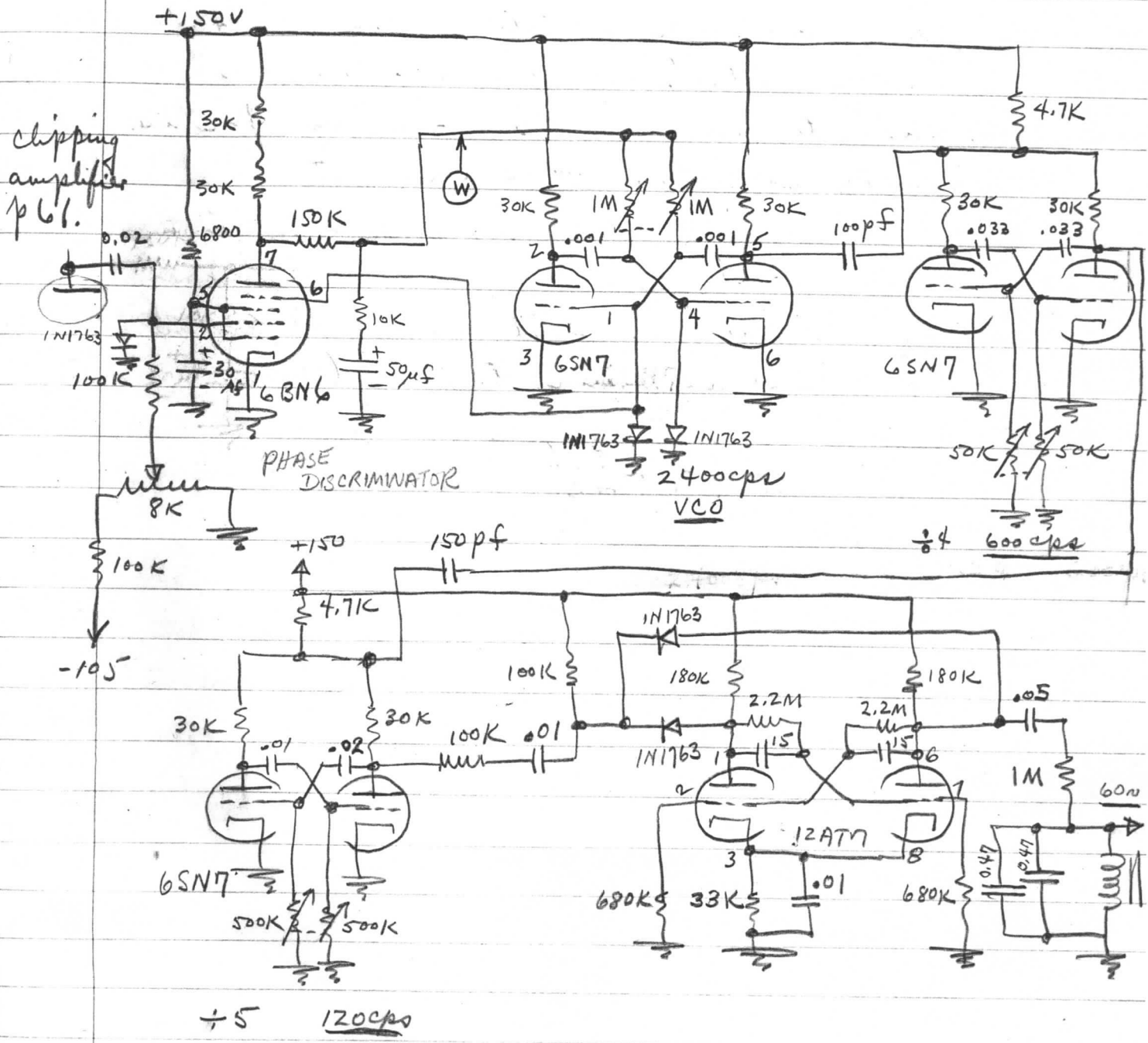
$$50\mu f R = 10 \text{ sec}$$

$$R_1 = \frac{10}{50\mu} = 200K$$

$$R_2 = 2K$$



Adding the break networks at \textcircled{Y} : Internal impedance for charging (200K) is too large considering the 300K set value of the 1M dual pot. Also; it locks up on a submultiple before it charges up the $50\mu\text{F}$ capacitor to the proper value - Changed 2K to 10K because loading decreased loop gain apparently. Actually works very well - it was not adjusted properly. Set $\textcircled{W} + 9.5\text{V}$ will hold on anything that can be heard in the noise. Set to be stable on noise it held very well through an entire pass from first audible tone to last - including frame bursts (not a wiggle) and several short disappearances of the signal.



5/10/65 : To save money on film and to use enlarger to simplify scale adjustments to match a map scale, the recorder drum diameter can be cut to 1" — Picture width will be 3.14". If I cut an 8x10" film into two 4x10's — setting picture length at 3.14" — I can get

$$\frac{10''}{3.14''/\text{frame}} = 3.2 \text{ frames in the length}$$

This is about the length of one pass. 6:1 improvement in film cost. Will need

$$\frac{3.14''}{3.5 \text{ min}} \times \frac{24 \text{ rev}}{\text{in}} = 21.5 \text{ RPM}$$

Hurst has a 20 RPM motor — (16-20-24)

If I used the 10-32 threaded stocks

$$\frac{3.14 \text{ in}}{3.5 \text{ min}} \times 32 \frac{\text{rev}}{\text{in}} = 28.8 \text{ RPM} \quad (\text{Hurst has 25 \& 30})$$

5/15/65

Audio oscillator p 51. I had used a 10K resistor on one 6SK7 to ground instead of 1M. Changed also to a 3W lamp but the time constants were wrong and it squegged at about $\frac{1}{3}$ cps. Back to 6W. Recalibrated. Waveform very good now but the dual 1M pot still gives some trouble, apparently due to loose mechanical coupling (backlash) between sections and lack of precise resistance tracking.

I have made no pictures since I improved the video frequency response and built the 2400 cps countdown chain.

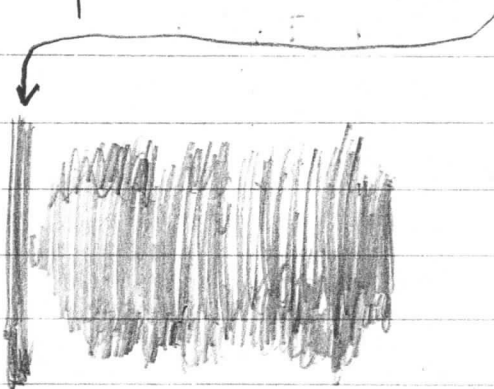
Considered changing the $\div 5$ stage to $\div 4$ and $\div 6$ by a switch to help in synchronizing but the run-through rate would be 1 line per second and $\frac{2}{3}$ line per second which is too fast. Easiest might be to use a variable frequency oscillator in place of signal in phase locked loop -

Reinstalling recorder after taking it to AED Hightstown for pictures - noted that imaged size of AR3 is .0032" (see p 45) - added small lens 7.5 mm diam 18 mm focal length ahead of eyepiece (about $\frac{1}{2}$ ") and cut image size in half - $\left(\frac{6''}{800 \text{ lines}} = 0.0075''\right)$ - now have about .016"

5/17/65 Made two new negatives yesterday. Cuba and the picture after it. The phase lock held and gave extremely straight edges -

Before taking the pictures built the 4pps sweep generator again, driving from the magnetic head pickup Schmitt.

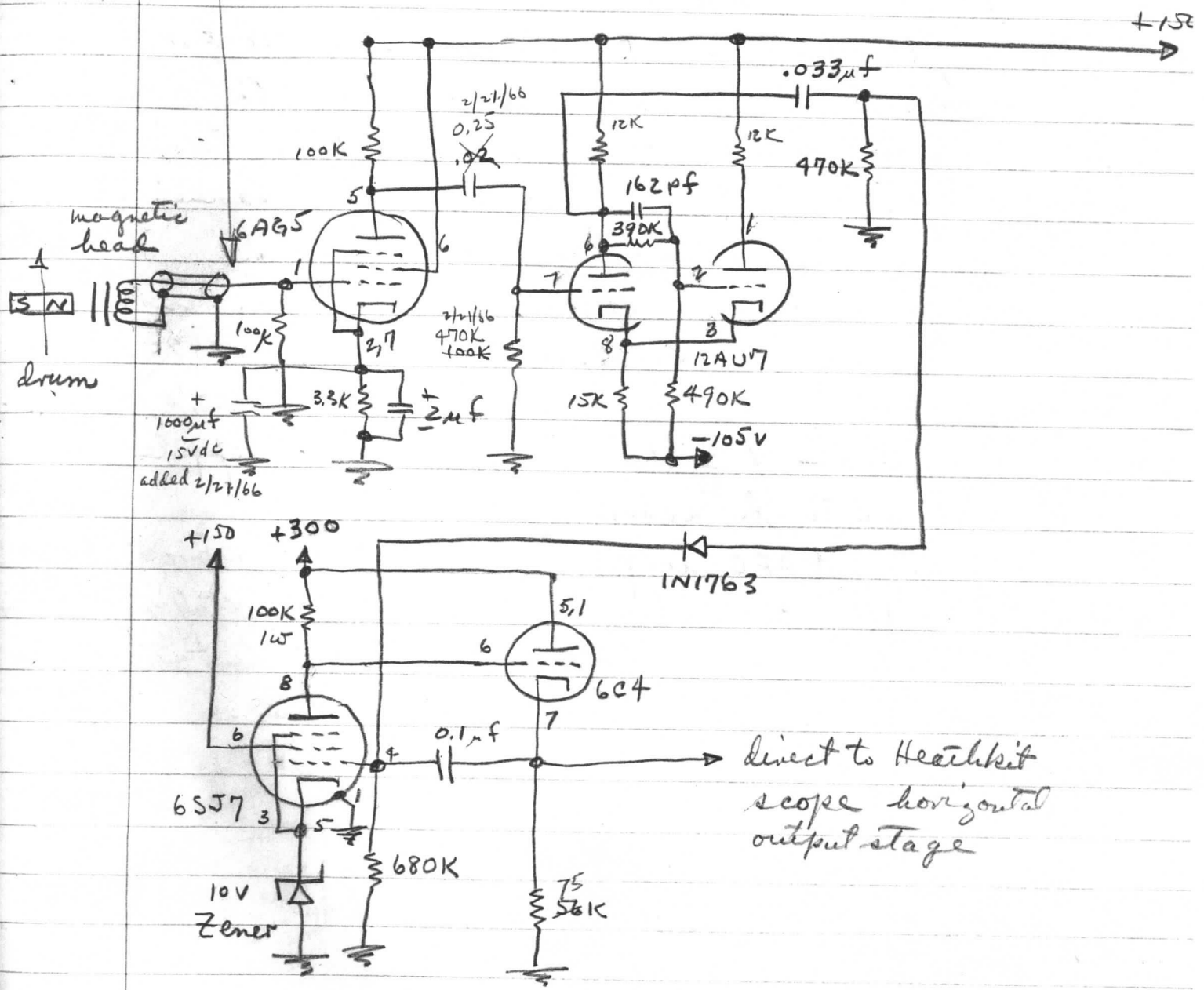
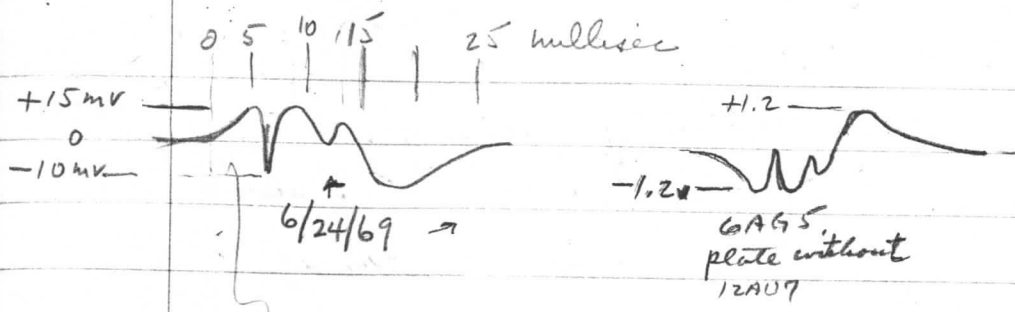
Monitoring video at ⑤ p61, observing position of retrace blanking pulse shows synchronism. For these pictures set blanking at beginning of trace



no Z axis modulation

See p 75 re sticking
Have some 5-line grouping, and traverse is sticking occasionally. Needs realignment and talcum.

Sweep drifts horizontally - probably poor resetting.



$$\begin{array}{r} 136.950 \\ 136.499 \\ \hline .451 \end{array}$$

5/18/65 From p 56 - In considering tracking methods, I had been assuming that ~~my~~ FM IF would be used for signal while the normal AM IF would be used to recover the conical scan on the signal. This is not practical since the FM carries the signal out of the AM pass band. FMFB

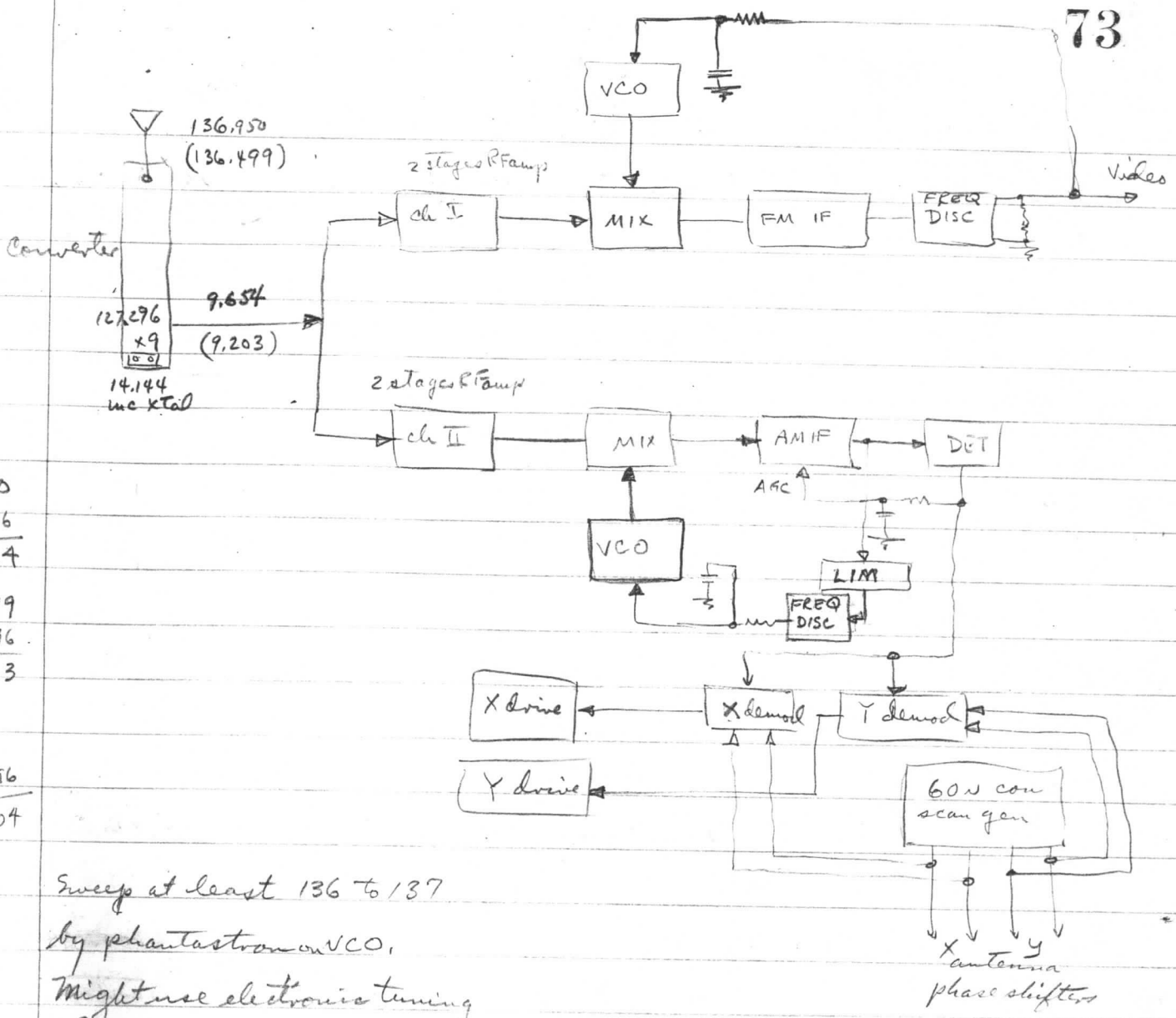
The most elegant approach would be to track beacons and have a separate signal channel. The signals can be a megacycle apart.

From the catalog of objects in orbit: The Nimbus I beacon is at 136.499 mc. $136.950 - 136.499 = 451 \text{ Kc}$

(I can easily get into problems with 2 L.O.'s)

Also - if 2 channels are used - Doppler will have to be accommodated on each -

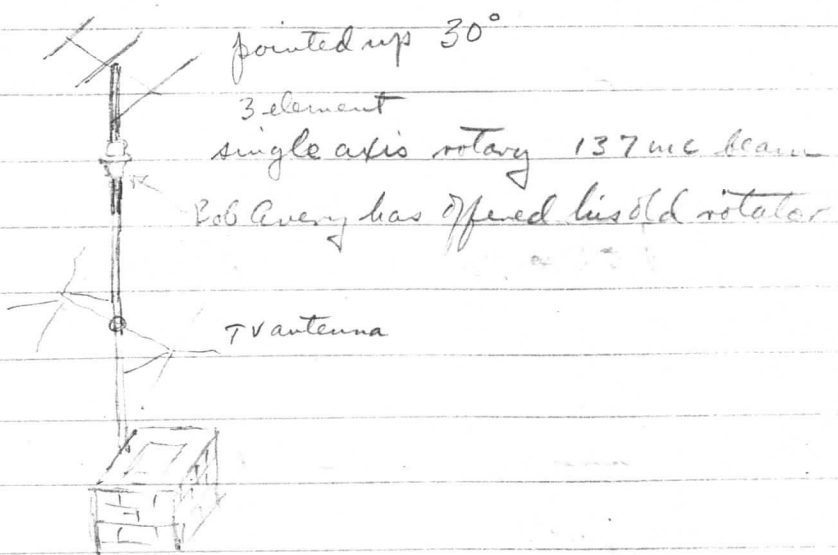
I could put AFC loops on each - This approach would permit my keeping my present xtal oscillator in the converter and would give independent operation and permit other converters for other bands later.



$$\begin{array}{r} 136.950 \\ 127.296 \\ \hline 9.654 \\ 136.499 \\ 127.296 \\ \hline 9.203 \\ \\ 136 \\ 127.296 \\ \hline 8.704 \end{array}$$

Sweep at least 136 to 137
 by phantastron or VCO.
 Might use electronic tuning
 for manual. Set sweep
 width by dial selection
 on top of manual.
 This requires RF amps to
 be as wide as widest
 sweep ^{with} ~~using~~ phantastron
 always sits off freq -
 could kill it by dc from
 disc center.

5/19/65



Installation to give signals for RF experiments. To set up the beam, I need VSWR bridge and signal source.

5/20/65

Normally I really don't need a sweep as wide as 1 mc. More like 20 kc -

If I used the 4pps sweep generator triggered from the rolling pin, I could get some very nice post detection integration, show doppler, etc. The $3\frac{1}{2}$ min sweep might be OK for some purposes but not long enough for an orbital pass - Wonder if that motor could be pulsed to slow it down - Probably would be too load-dependent. One revolution is 5 lines.

For 20kc sweep at 4 sweeps/sec rate is $\frac{20\text{kc}}{\frac{1}{4}\text{sec}} = 80\text{kc}^2/\text{sec}^2$

The rise time of a filter is about $\frac{1}{\Delta f}$ - Max sweep rate
 is $\frac{\Delta f}{1} = \Delta f^2$

$$\Delta f_{\min} = \sqrt{80,000(\text{cps})^2} = 280 \text{ cps}$$

5/31

6/1/65 Ran 3 pictures yesterday - Two major
 developments - the 10 volt level
 at monitor point is in saturation enough
 to wash out high level detail - Cuba picture
 is much better at 7 volts peak-to-peak at
 (5) of p61. - Also - found that the line
 pairing previously attributed to irregular \leftarrow (p70)
 drive is actually due to shifting of the
 AR3 discharge.

(6) Image of AR3 in 20X microscope

I reoriented the lamps to (DD) and took 5/31/65 (C)
 (not yet developed).

I am now in a position to make a picture
 with the Goddard tape dub.

Goddard Tape:

Set to zero at start of noise in orbit 341

First frame 085 well modulated video

2nd frame 156 noise at 128 and end at 180

204 begins again gets noisy immediately, good at 223

Frame at 242 noisy gets better good at 301

" " 319

" " 400 noisy 468 end 471

mark "orbit 342" means "end of orbit 342" apparently

Made and developed Goddard Cuba picture

6/2/65

Goddard tape signal to noise ratio is very much better. The signal also starts and stops very abruptly a few seconds from ^{above} threshold to complete dropout. They do have a few fades in odd places but their pictures are very clean.

Phase lock held through a complete fade at the start of the Cuba picture.

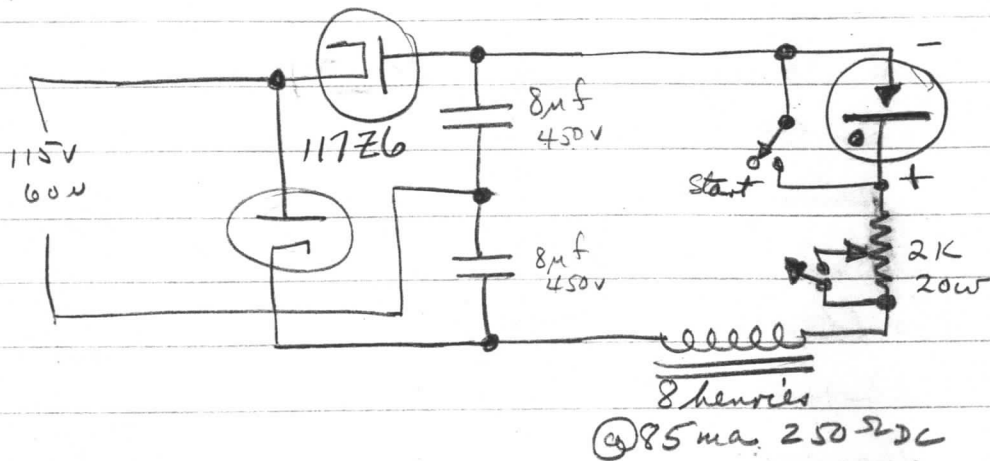
I should recheck orientation of the AR 3 - it may have slipped. The pictures show slight line pairing. Ultimately I will have to use the arc lamp to get pictures without dots where the discharge changes. Resolution will also be better probably since the AR 3 image is still too large

6/4/65 It should be possible to approximate the optimum design of RF amplifiers and multipliers using the data of pp 385-6 of Radio Engineering by Terman. The optimum conduction angle of a multiplier should follow from the order of multiplication and will be less than for a straight amplifier.

6/5/65 Electronic news reports Gemini GT4 frequencies 296.8 mc and a trial HF freq of 15.016 mc. Duplication is that 2 channels near 296.8 mc are used, one for backup.

16 m/s x v d e w c c → o b e g a x 2 8 1 2 a n d
2 8 1 2 a n d

Recommended circuit from Edmund's Scientific
for Zirconium Arc Lamp. Stock no 40,531



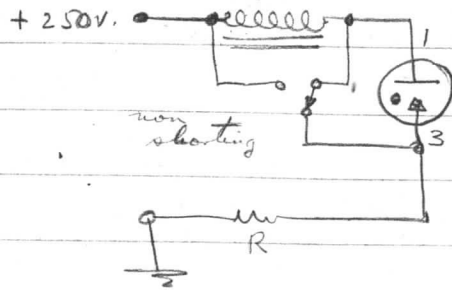
Lamp characteristics

2 watt 38 volts 55 ma, 200 volt min supply,
1000 volt minimum start. Mean light source diam = 0.005"
Avg brightness 25 candles/mm² - Avg axial candle power = 0.3
Mean candle power per watt 0.13. Avg lumens in 90° angle 0.47
Bulb type T5 max temp °F bulb 140°F base 100°F avg life 150 hrs.
Color temperature 3200°K

Base pin #1 positive

pin #2 no connection

pin #3 negative



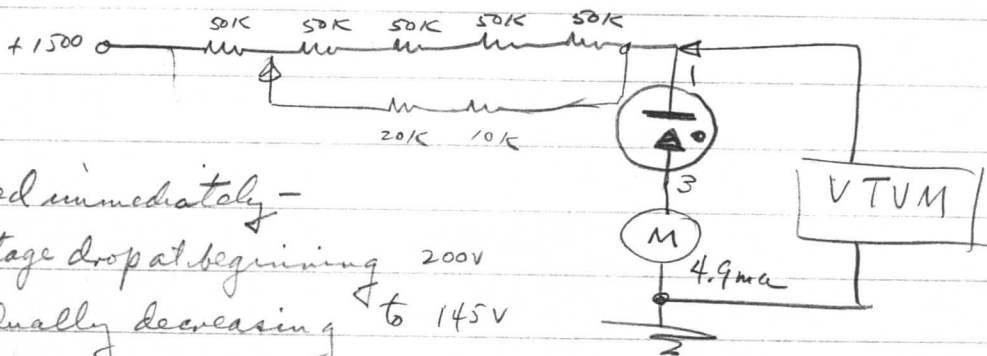
Say 70ma $R = 25K$ 2.5watts.

6/8/65

Using a variety of chokes and running the stored current up to 60ma was not able to strike the arc. I used a relay to break the circuit. Measuring on the scope, I never got above 1,000 volts. Next approach should be to use HV supply from Xutro.

6/13/65

Using the transmitter supply + 1500V at no load



Fired immediately -
voltage drop at beginning 200V
gradually decreasing to 145V
after 10min.

Also fires with 300K across lamp - indicating a 750V threshold. This was measured immediately after 15 mins of operation (1140AM)

The current through the lamp and voltage across when fired are apparently related as a negative resistance - voltage across lamp goes up when supply is turned off - 45 min later still fires w/ 300K in parallel.

The stability of the discharge seems to be quite poor. Hysteresis is readily apparent - Repeatability problems are evident. Apparently the discharge generates considerable RF - can pull a $\frac{1}{4}$ " pale blue arc in the resistor networks - Tried bypass with .01 and 1K and .01 and 100 Ω but can still pull arc. Perhaps slightly more stable but cannot be sure.